



## Hot Forming



## Diffusion Bonding

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# Biaxial hot forming of AA2219 with SPF and other hot forming processes

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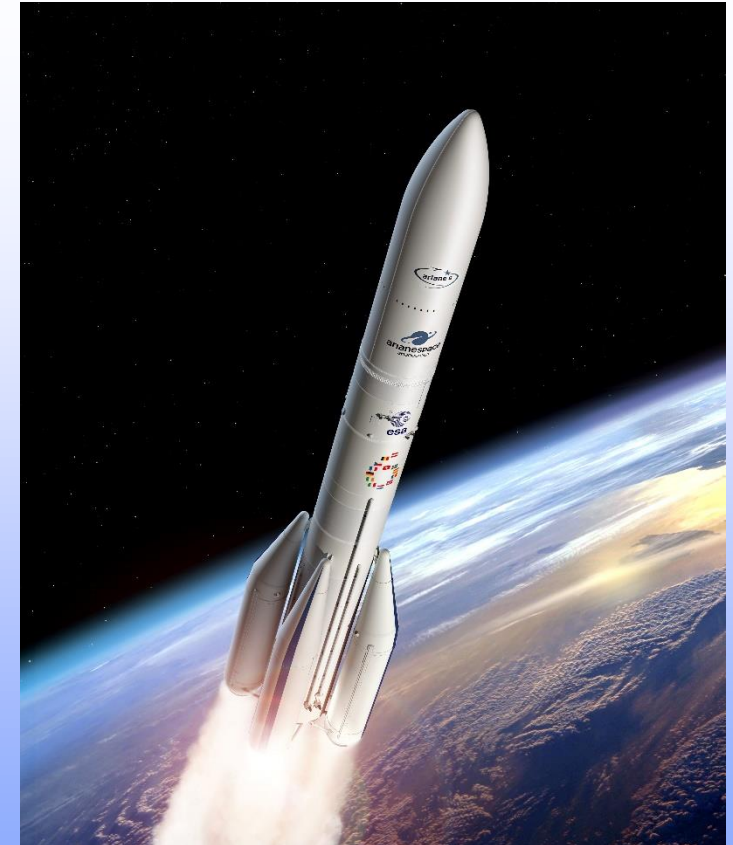
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## Advanced forming technologies for complex shapes

Development, manufacturing and test of new structural tank demonstrators for ARIANE 6 from AA2219

Consortium:

1. MT-Aerospace, Germany, Design and production of tank body
2. Omnidea-RTG, Germany, Project management
3. Omnidea Ltd., Portugal, Incremental forming of tank dome with magnetic pulse process
4. FormTech GmbH, Germany, Hot forming of tank dome



# Hot forming of sheet metal AA2219

State-of-the-art / literature:

„Superplastic Blow Forming of AA2219 Aluminum Alloy“

R.Kaibyshev, I.Kazakulov, D.Gromov, D.R.Lesuer, T.G.Nieh

Summary:

- AA2219 = Al6,4Cu0.3Mn0,19Zr0,0,6Fe
- Material from special TMP treatment
- Investigation on ultrafine grain size (GS)  $\sim 12 \mu\text{m}$ ~ASTM 9,5
- Test parameters: 450-540°C,  $p_{\text{SPF}}$  0,2 to 0,4MPa,  $\dot{\varphi} = 2,2 \times 10^{-5}$  to  $1,1 \times 10^{-1} \text{s}^{-1}$
- Cone tests with and without backpressure
- Max achieved strain  $e=670\%$
- Max strain at 500°C and  $\dot{\varphi} = 2,2 \times 10^{-4} \text{s}^{-1}$  under backpressure
- Lot of cavities without backpressure
- Very few cavities with backpressure

# Project challenge

- Information from literature hardly transferable due to much coarser GS of standard sheet and plate material
- Application requires forming of a thin membrane inside a thick plate
- Thickness ratio „ring“ to „membrane“ is 100 to 5%
- Required bottom curvature is „Cassini shape“
- Part shape requires thickness strain of minimum  $\sim e = 21\%$ ,  $\phi = 0,24$  assuming constant wall thickness in formed region
- Cavities and „open porosity“ not acceptable for the application

## Simplified approach:

- Test samples from standard sheet metal
- Validation of SPF, HDD, HSF process capabilities
- Metallurgical examination regarding cavities
- If one HF process possible: Application on „like-real“ blanks with „plate“ ring and machined „membranes“

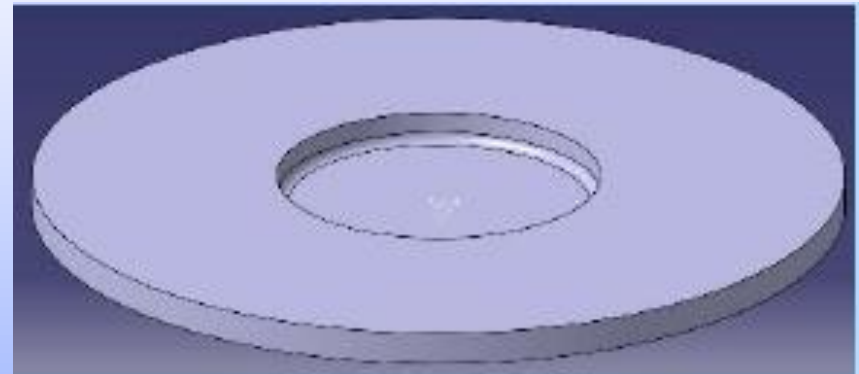


Plate material and machined membrane

# FormTechs' equipment for HF processes



FT's R&D equipment is suitable for  $T_{\max} \sim 1.100^{\circ}\text{C}$ ,  $p_{\max} = 6\text{MPa}$ , Max ram force 100t

- SPF (superplastic- / gas pressure forming)
- HDD (hot deep drawing),
- HSF (hot stretch forming)

SPF with single action press

HDD and HSF with double action press.

- Double action press is unique. Built in alliance with



Evaluation of process parameters

- „Cone“ for SPF
- „Swift“ for HDD and HSF

R&D actions:

Phase 1:

Standard sheet metal available in  $t_s = 2\text{mm}$ , GS= ASTM 4-5

Phase 2, not yet finished/ results pending:

Forming of membrane machined down from plate material

$t_p = 40\text{mm}$

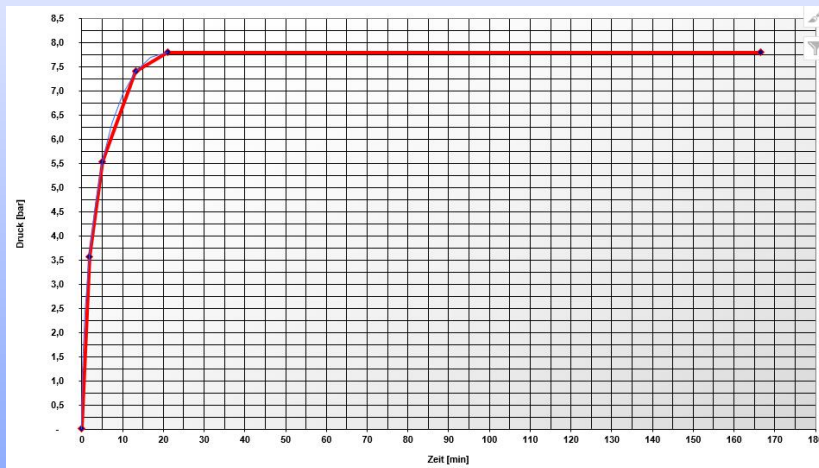


Material AA2219-O,  $t = 2,03\text{mm}$   
provided by MT-A



# Gas pressure forming/“SPF” of AA2219

- SPF temperature for AA2219:  $\sim 500^{\circ}\text{C}$
- Variation of applied pressure-time-curve incl. back pressure
- Test result: Cone height 100% or premature failure

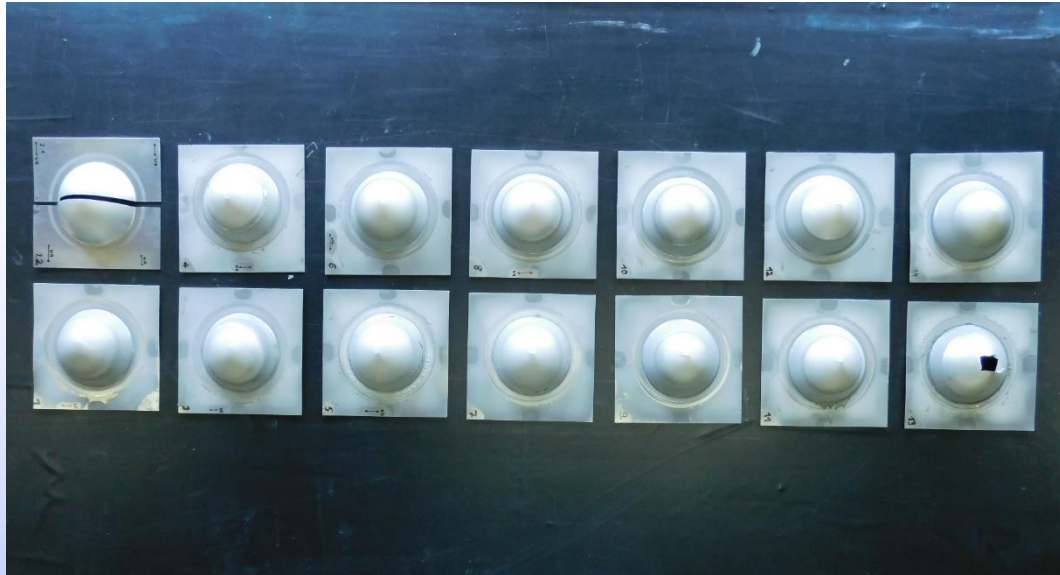


Example: time-pressure-curve



Sample cone Ti6-4 at  $\sim 850^{\circ}\text{C}$

# Test parts AA2219

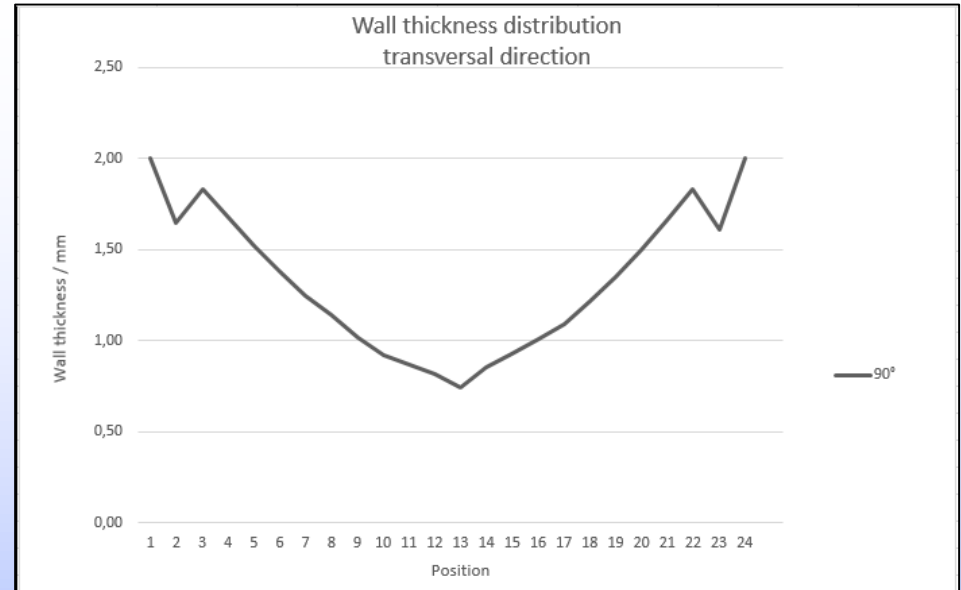
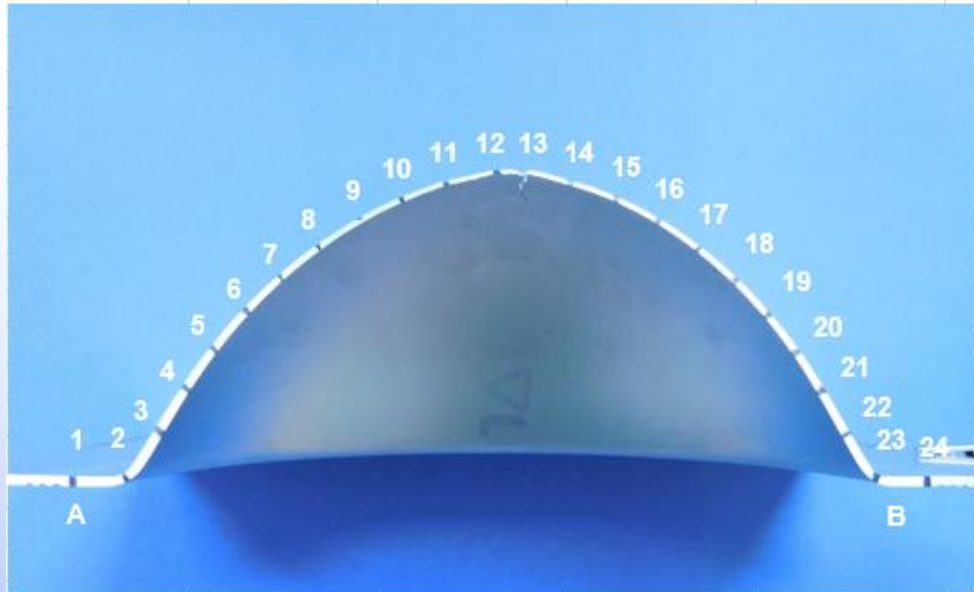


14 samples with and without backpressure

Extraction of microsections



# Wall thickness distribution



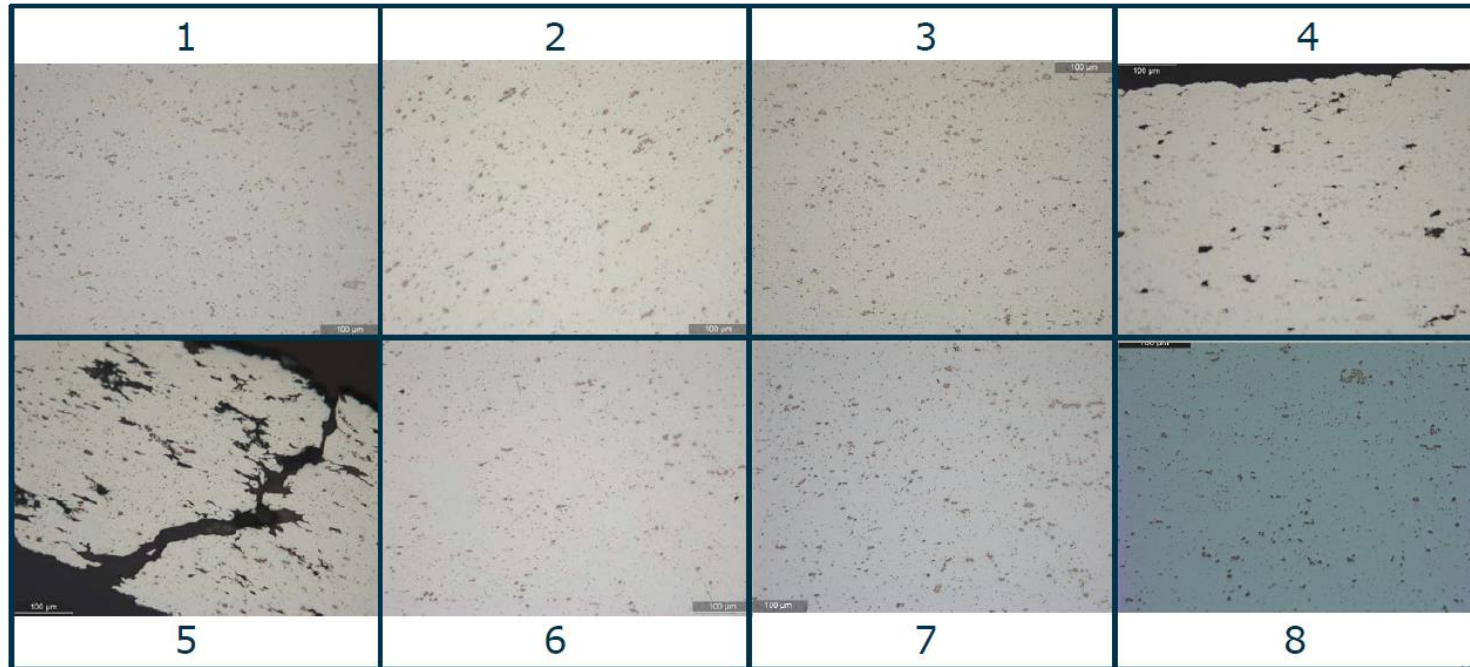
## Wall thickness distribution:

- Minimum wall thickness of 0,74mm in pole near crack
- ~Linear reduction of wall thickness from radius to pole
- Failure initiation from cavities even with high back pressure



# Micrographs of cone sample No 14

Sample V14 (Cone)



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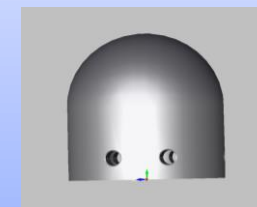
Cavities at strain  $> \sim \epsilon = 0,2$

Requirement no cavities at  $\epsilon \geq 0,24 \rightarrow$  not achieved

SPF process with standard sheet not feasible

# Test program HDD/HSF

- Definition of HDD process parameters
  - Constant wall thickness
  - Suitable forming temperature
  - Sufficient formability / cup height?
  - Forming without cracks
- Definition of lubricant
  - Smooth surface
  - No abrasion of tool and part
- Sufficient drawability
  - SWIFT – flat bottom
  - Hemispherical bottom
  - Cassini shape bottom
- Definition of HSF\* process parameters
  - Controlled material flow of blank over curved punch head!!



Different punch geometries:  
Flat, hemispherical  
and Cassini shape

\*HSF ~ HDD without material from flange area

# Test samples HDD/HSF



# Forming temperature for HDD of AA2219

No. of samples	Blank diameter	Punch geometry
20	180	flat



Typical view of deep drawn cups

Temperature range: 180°C – 450°C

Result: Best formability/ highest cup at T= 230-240°C

Good repeatability.

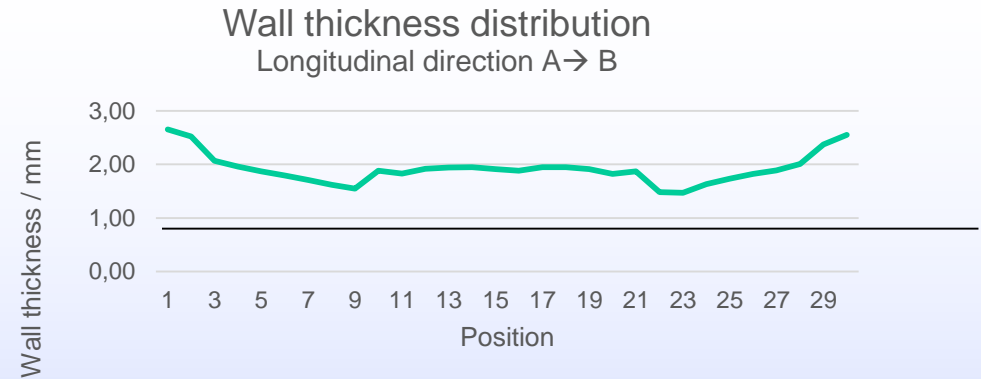
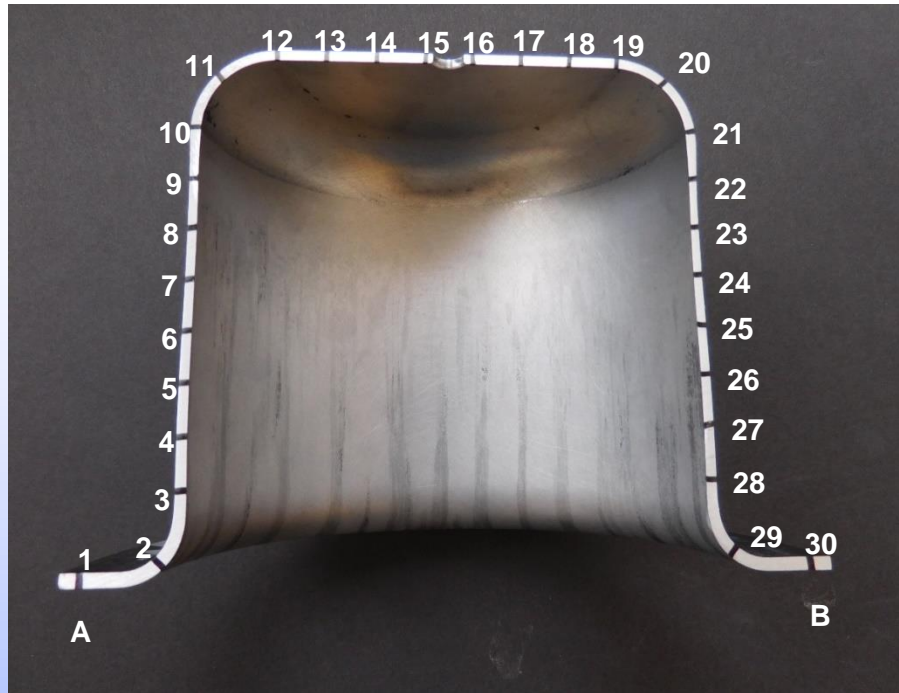
Cracks in usual position: Short below bottom radius

Wall thickness near cracks  $t \sim 1,4\text{mm}$

→ Critical thinning ratio for crack initiation:  $\epsilon \sim 0,37$



# Wall thickness distribution HDD



## Wall thickness distribution:

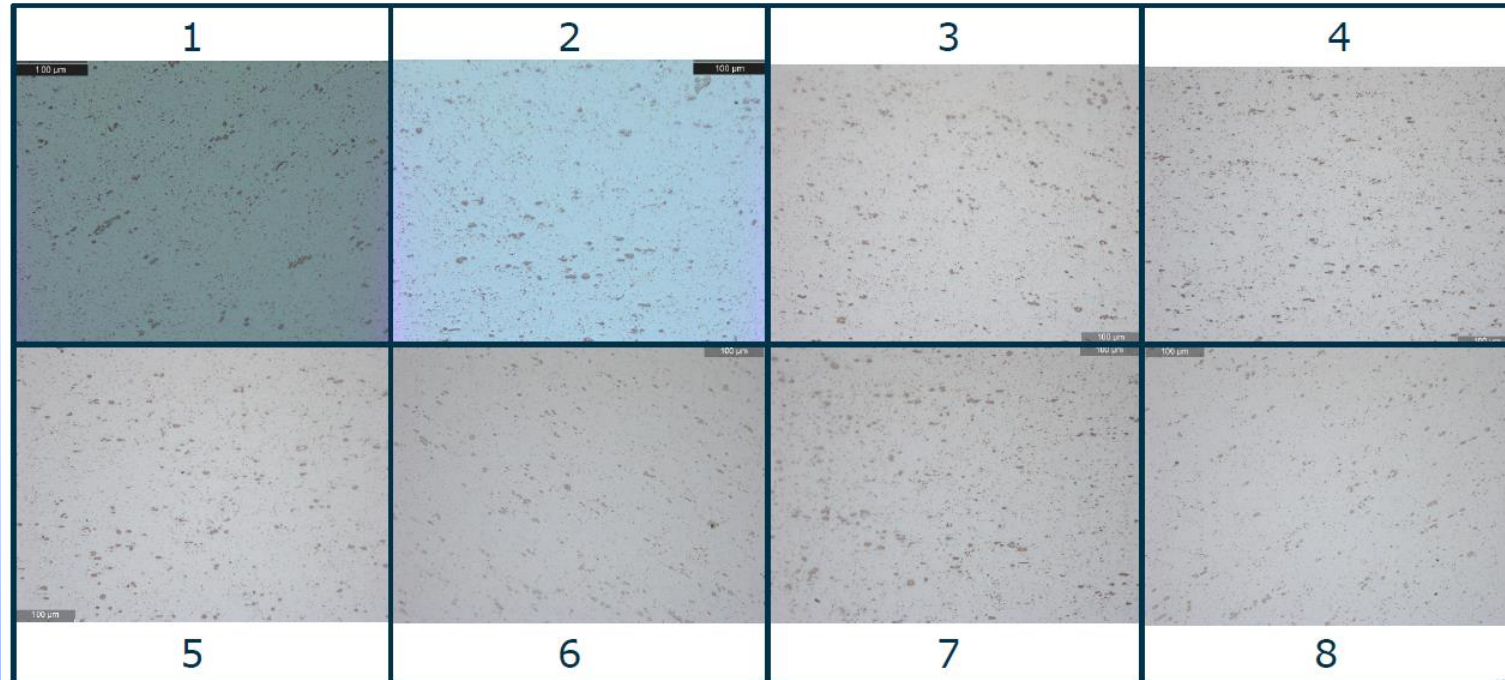
- Thickening up to 0,65mm in the flange area
- Wall thickness
- Bottom area:  $\sim T_{const}$
- Cup walls: decrease linear, minimum  $t \sim 1,47\text{mm}$ , see 8/9 and 22/23





# Micrographs HDD sample

Sample 39 (Cup)



HDD seems to show no cavities. Doubts be checked with SEM  
Unfortunately HDD only possible with uniform blank thickness

# Hot stretch forming

No. of samples	Blank diameter	Punch geometry
30	240	Cassini

Dome forming of machined membrane from plate material

- “No” material flow from flange possible due to “ring”
- Forming of Cassini dome curvature from flat blank requires stretching of membrane = thinning
- Acceptance level of test bodies → similarity to real shape
- Required dome height=28mm

Test results:

- H=28mm(+) achieved.
- Min t=1,44mm
- Surface doesn't show excessive signs of necking

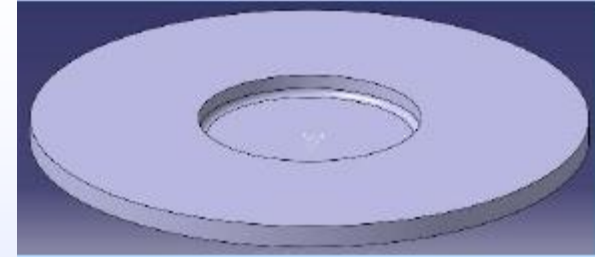


Plate material and machined membrane

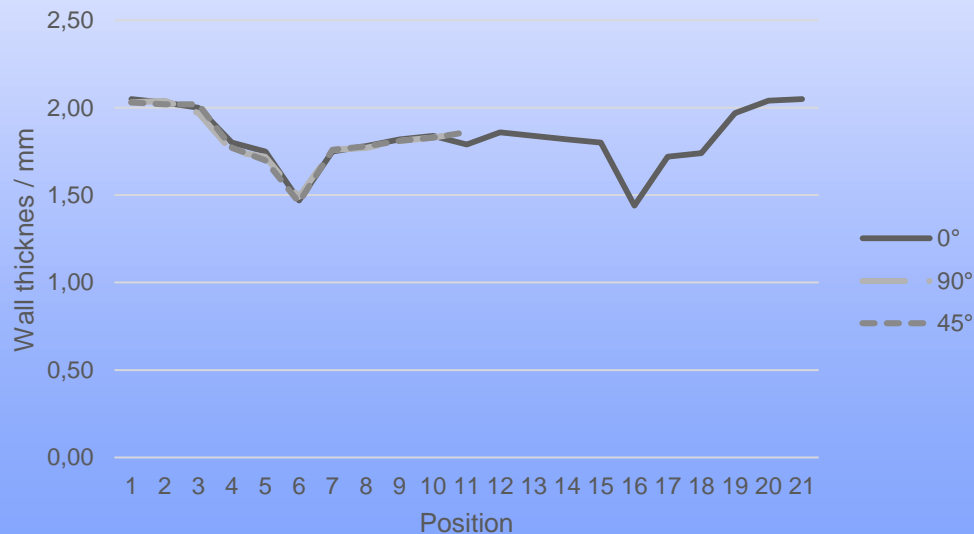


Hot stretch formed part R28 with Cassini bottom

# Wall thickness distribution HSF



Wall thickness distribution



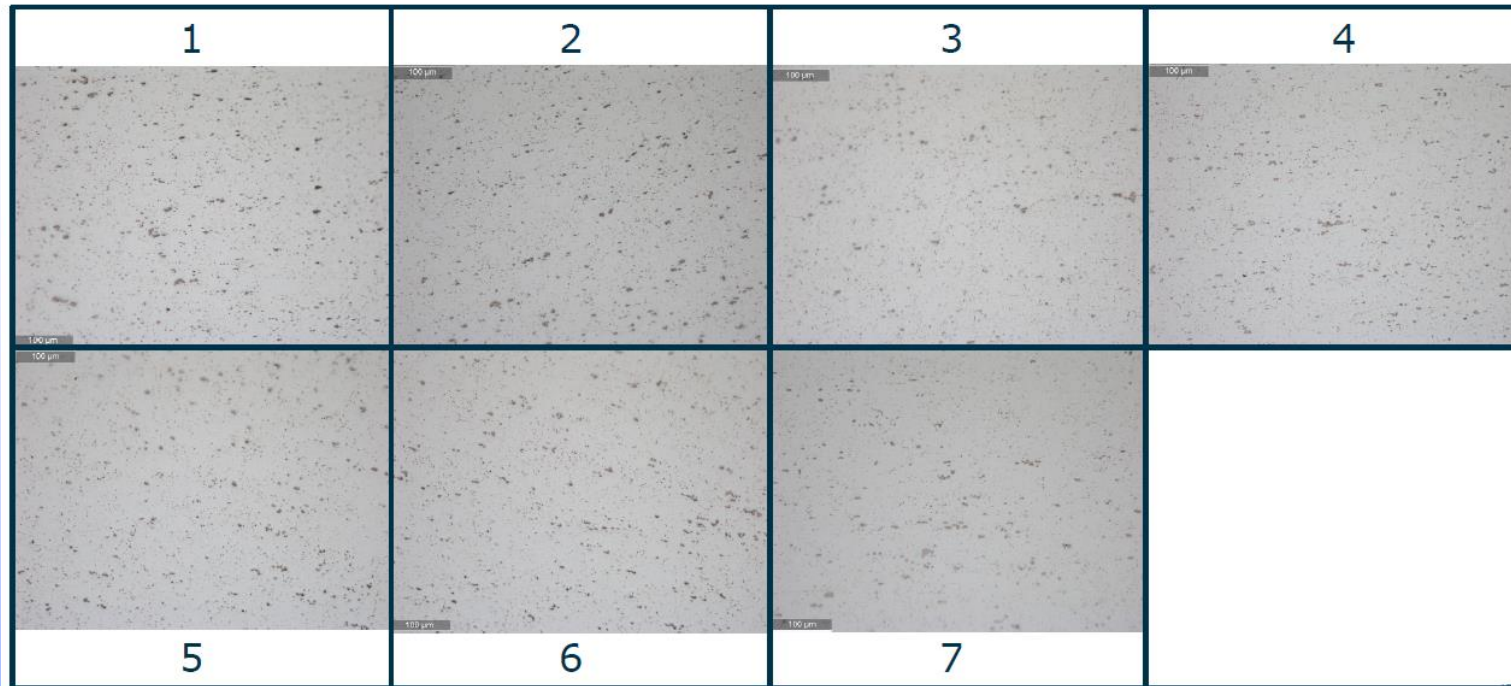
Wall thickness distribution:

- No variation on wall thickness in clamped area (pos. 1-3 and 19-21)
- Approximately constant wall thickness in the Cassini-shape bottom area (pos. 7-15)
- Minimum wall thickness  $t=1,44\text{mm}$  just below bottom radius (pos. 6 and 16)
- $\epsilon \sim 0,34$  is near to necking
- No anisotropy visible



# Micrographs HSF

Sample R27 (Cassini)



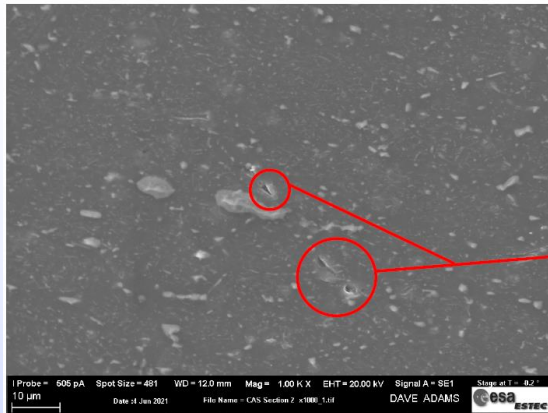
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HDD seems to show no cavities. Doubts be checked with SEM as with HDD  
HSF seems possible with „real“ blank geometry



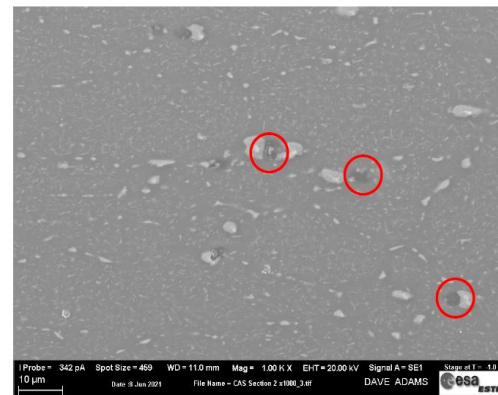
# SEM results HDD and HFS

## SEM Analysis - Cassini Sample, Position 2



- Coarse intermetallic phases
- Some grain boundary precipitates
- Occasional pull out of intermetallics
- No evidence of any small pores

## SEM Analysis - Cassini Sample, Position 2



Small pores seen in optical metallography are in fact intermetallic particles that have been pulled out during sample preparation

Small voids visible in micrographs are not at all microcavities



# Distribution of pores. Summary SPF, HDD, HSF

## Summary – After Metellography + SEM Analysis



Sample	Analysis Position							
	1	2	3	4	5	6	7	8
Cone 2.1 (SPF)	Green	Green	Yellow	Orange	Yellow	Green	Green	Green
Cone H3 (SPF)	Green	Green	Orange	Red	Yellow	Green	Green	Green
Cone V14 (SPF)	Green	Green	Green	Orange	Yellow	Green	Green	Green
Cup 39 (HDD)	Green	Green	Green	Green	Green	Green	Green	Green
Cassini R27 (HSF)	Green	Green	Green	Green	Green	Green	Green	Grey

No Pores    
  Occasional Pore    
  Many Pores    
  Very Bad



# Summary SPF, HDD& HSF of standard AA 2219



## **Gas pressure forming/ SPF**

Despite backpressure cavitation starts at  $\epsilon \sim 0,2$

**→ Dome forming of given application with gas pressure forming/ SPF not possible**

## **HDD**

HDD of sheet metal performed successfully with flat, hemispherical and Cassini-shaped punch

AA2219 hot deep drawing ratio is exceptionally good  $\rightarrow \beta_{\max} \geq 2,4 = \text{max achievable}$

**→ HDD process of thin membrane machined inside thick plate not possible**

## **HSF**

HSF successfully demonstrated for the real application, but with sheet metal blanks instead of machined plate

**→ tbd if even coarser microstructure of membranes machined from plate will work**

**→ HFS with samples from plate material to come**

Thank you very much for your attention

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